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# Phase Diagrams and Morphology of a Urethane Model Hard Segment and Polyether Macroglycols

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ABSTRACT: Binary mixtures of a urethane hard-segment model compound, diethyl 4,4'-methylenebis(Nphenylcarbamate) (H<sub>1</sub>), and various polyether macroglycols have been investigated by means of differential scanning calorimetry, wide-angle X-ray diffractometry, and optical microscopy. Both poly(ethylene oxide) (1500 MW) and poly(tetramethylene oxide) (1000 MW) form a eutectic with  $H_1$  in weight ratios of  $H_1/PEO$ (40/60) and  $H_1/PTMO$  (20/80). Poly(propylene oxide) and  $H_1$  mix to form a crystalline-amorphous blend. X-ray diffraction patterns showed that the presence of polyether macroglycols caused no change in the crystal structure of H<sub>1</sub> crystals in the blends. This suggests that the melting point depression observed is explicable in terms of H<sub>1</sub>-polyol thermodynamic mixing. On the basis of Scott's equation, the interaction parameter densities of  $H_1/PEO$ ,  $H_1/PTMO$ , and  $H_1/PPO$  were determined to be -4.63 cal/cm<sup>3</sup>, -3.42 cal/cm<sup>3</sup>, and -1.21 cal/cm<sup>3</sup>, respectively, at the  $H_1$  melting point. Optical microscopy revealed that  $H_1$  spherulites were larger in size and more perfect in texture in the blends of H<sub>1</sub> and polyols than in pure H<sub>1</sub>.

# Introduction

The morphology and physical properties of diphenylmethane diisocyanate (MDI) based segmented polyurethanes have been studied extensively<sup>1-4</sup> and have been found to depend on several factors such as the composition ratio of urethane and polyether segments, the molecular weight of the individual segments, and segmental compatibility.

In this study, the segmental compatibility of urethane hard segments and polyether soft segments was investigated by determining the phase diagrams of physical mixtures of a model hard segment with various macroglycols. Diethyl 4,4'-methylenebis(N-phenylcarbamate) (designated as H<sub>1</sub>), which is the repeating unit of the MDI-butanediol (BD) hard segment, served as the hardsegment model compound. Poly(ethylene oxide) (PEO), poly(propylene oxide) (PPO), and poly(tetramethylene oxide) (PTMO) macroglycols were used to model the soft segment.

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A recent study by Camberlin<sup>5</sup> showed that the hardsegment model compound diethyl 4.4'-methylenebis(Nphenylcarbamate) displays a melting point of 125 °C in its initial stable form and 99.7 °C in its metastable form. Blackwell<sup>6</sup> studied a similar model compound of the urethane hard segment, dimethyl 4,4'-methylenebis(Nphenylcarbamate), using X-ray diffraction. This model compound was found to possess a monoclinic structure with four molecules in each unit cell. However, he also reported an oriented MDI/BD hard segment in a triclinic structure.7,8

The crystalline structures of poly(ethylene oxide) (PEO) and poly(tetramethylene oxide) (PTMO) have been studied extensively by a number of authors using X-ray scattering and IR spectroscopy.9-12. PEO was found to possess a monoclinic helical structure with four repeating units in each unit cell, and PTMO was found to possess a planar zigzag monoclinic structure with two repeating units in Atactic poly(propylene oxide) is an each unit cell. amorphous material.

When two crystalline polymers or one crystalline and one amorphous polymer are mixed together, the miscibility of the two components with respect to composition and temperature can be represented in a phase diagram. In the analysis of polymer–polymer phase diagrams, Scott's treatment of polymer mixtures based on the classical Flory–Huggins equation is widely used to calculate the spinodal and binodal compositions and the melting point depression. <sup>13–16</sup> In this theory, the chemical potential  $(\mu_{2u})$  or activity  $(a_{2u})$  of a structure unit of component 2 in a binary polymer solution can be expressed as

$$(\mu_{2u} - \mu^{\circ}_{2u})/RT = \frac{V_{2u}}{V_{1u}M_2} \left[ \ln \phi_2 + \left( 1 - \frac{M_2}{M_1} \right) \phi_1 + \chi M_2 \phi_1^2 \right] = \ln a_2$$
 (1)

where subscript 1 represents the polymer which is considered as a diluent for polymer 2, and  $V_{2u}$  is the molar volume of the structural unit of polymer component 2.  $\phi_2$  is the volume fraction and  $M_2$  is the degree of polymerization of polymer 2, and  $\chi$  is the interaction parameter. The activity coefficient of the structural unit of component 2 in the mixture is expressed as

$$\ln \gamma_2 = \frac{V_{2u}}{V_{1u}M_2} \left[ \left( 1 - \frac{M_2}{M_1} \right) \phi_1 + \chi M_2 \phi_1^2 \right]$$
 (2)

The molar excess Gibbs free energy due to mixing can then be written as

$$G^{\mathbf{E}} = RT(\phi_1 \ln \gamma_1 + \phi_2 \ln \gamma_2) \tag{3}$$

where

$$G^{E} = H^{E} - TS^{E} \tag{4}$$

When  $G^{E}$  has a negative value, mixing is thermodynamically favored.

In this work, phase diagrams of three binary mixtures of a urethane hard-segment model compound,  $H_1$ , and polyether soft-segment model compounds, PEO, PPO, and PTMO, were analyzed. The interaction parameter density, B, in the blends was determined from the depression of the hard-segment melting point. Wide-angle X-ray diffraction was used to analyze the diffraction characteristics of the  $H_1$ -polyol blends at various compositions and temperatures. In addition, the effect of composition on the spherulite size of the crystalline blends at a given temperature was studied using a polarizing optical microscope.

### **Experimental Section**

Materials. The materials studied include diethyl 4,4′-methylenebis(N-phenylcarbamate) (coded H<sub>1</sub>) and its blends with three polyethers of different oxygen to carbon ratios. These are poly(ethylene oxide) (PEO) of 1500 MW obtained from Aldrich, poly(propylene oxide) (PPO) of 1000 MW obtained from BASF Wyandotte, and poly(tetramethylene oxide) (PTMO) of 1000 MW obtained from Quaker Oats. The hard-segment model compound (H<sub>1</sub>) was made by capping MDI with ethanol. The synthesis was carried out by stirring 4,4′-methylenebis(phenyl isocyanate) with excess ethanol at 50 °C. As the reaction proceeded, H<sub>1</sub> precipitated as a white product. After an IR trace showed that no isocyanate residue remained in the ethanol solution, the model compound was collected by vacuum filtration. H<sub>1</sub> was dried in a vacuum oven at 50 °C for 1 week and its purity assessed by NMR and gel permeation chromatography.

Blends of  $H_1/PEO$ ,  $H_1/PPO$ , and  $H_1/PTMO$  were prepared from dilute THF solutions (1% by weight). The THF was slowly evaporated at room temperature to allow the components to mix at close to equilibrium conditions. A week was normally allowed

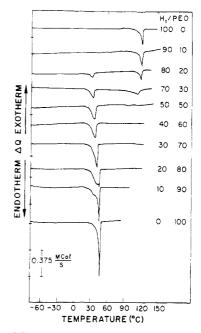


Figure 1. DSC thermograms of  $H_1/PEO$  blends.

for precipitation and mild drying of the blends. The blends were further dried under vacuum for 2 weeks at 25 °C.

Characterization. Density Measurement. The densities of the hard-segment model compound  $(H_1)$  and soft-segment polyols in their molten states were measured by a pycnometer using ASTM method D-70. The volume of the pycnometer was calibrated with mercury at various temperatures.

Differential Scanning Calorimetry (DSC). DSC measurements were conducted on a Perkin-Elmer DSC-2 which was calibrated with mercury and indium standards to  $\pm 0.2$  °C. The melting point of the pure materials and their blends were defined by the onset of the melting endotherms. The liquidus point of the blends is reported as the minimum in the endothermic melting peak. A heating rate of 5 °C/min under a He atmosphere was used in all cases.

Wide-Angle X-ray Diffraction. Wide-angle X-ray diffraction (WAXD) experiments were performed on  $\sim\!0.5\text{-mm}$  thick solvent cast samples with a Picker Model 3667A diffractometer. A sealed X-ray tube generator with a Cu K $\alpha$  target ( $\lambda$  1.542 Å) which operated at 35 kV and 15 mA provided the source of X-rays. Data were obtained from 3° to 40° with a time constant of 1 s. The slit system used had a Gaussian weighting function with a 1° full width at half-maximum. Intensity was plotted as counting rate vs. angle on a strip chart recorder.

Optical Microscopy. Spherulites were photographed with a Polaroid camera attached to a Carl Zeiss polarizing microscope. Samples were cast on the surface of glass plates and dried in a vacuum oven in a similar fashion to those prepared for thermal analysis.

## Results and Discussion

Thermal Analysis. Differential scanning calorimetry was used to determine the phase diagrams of blends of the polyols with the hard-segment model compounds. In each system, the composition ratio of  $H_1/\text{polyol}$  was varied from 100/0 to 0/100. DSC traces of the three systems studied are shown in Figures 1–3. The thermograms of each blend were recorded from –100 to 135 °C at a heating rate of 5 °C/min. Various heating rates (20, 10, 5, 2.5, and 1.25 °C/min) were first used on selected blends of  $H_1$  with the polyols. At 5 °C/min the effect of heating rate on the thermal transitions in the blends begins to level off. This heating rate, which allows reasonable sensitivity and rate of testing, allows the molecules in the blend to redistribute close to their equilibrium compositions with respect to the variation in temperature.

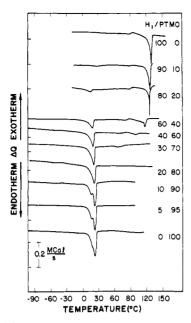


Figure 2. DSC thermograms of H<sub>1</sub>/PTMO blends.

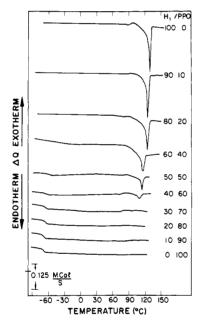


Figure 3. DSC thermograms of  $H_1/PPO$  blends.

Figure 1 shows the thermograms of the  $H_1/PEO$  system. The melting point of pure H<sub>1</sub> appears at 128.5 °C, which is in close agreement with the 128 °C obtained by Nakayama. 18 Recently, a  $T_{\rm m}$  of 125 °C has been reported by Camberlin.<sup>5</sup> In the thermogram of H<sub>1</sub> a small endotherm was observed at 87 °C, immediately followed by an exotherm at 97 °C. This is believed to be due to the melting and recrystallization of H<sub>1</sub> semicrystalline regions in which defects are present. These lower temperature thermal events can be eliminated by annealing at 77 °C for 10 min. As PEO was blended into  $H_1$ , the temperature range of the small endotherms and exotherms due to H<sub>1</sub> as well as its sharp melting point decreased. When the amount of PEO added was greater than 20% (wt %), a lower melting temperature was observed at 31 °C. The onset of this second  $T_{\rm m}$  appeared at the same temperature regardless of the variation in composition, and its area became larger as the concentration of PEO increased. It was also observed that the melting point of the hard segments and the peak area associated with it decreased as the hardsegment content decreased. This melting point completely

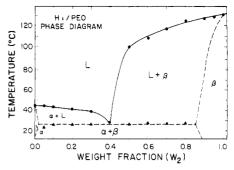


Figure 4. Phase diagram of the H<sub>1</sub>/PEO blend system. Liquidus points are shown by circles, and eutectic points by triangles. The solidus lines at both ends of the phase diagram are estimated.

disappeared at the composition of 40/60 (H<sub>1</sub>/PEO). With a further increase in the amount of PEO beyond 40/60 (H<sub>1</sub>/PEO), a new melting point appeared immediately following the 31 °C melting point. In the range of 30/70 to 10/90 (H<sub>1</sub>/PEO), these two melting peaks overlap to some extent. The area of the higher temperature melting peak increased with increasing amount of PEO. Finally, pure PEO displayed a melting point with an onset at 45 °C and peak maximum at 47 °C.

It is typical that binary mixtures giving rise to eutectic phase diagrams exhibit two melting peaks. 19 The rather sharp lower temperature endotherm, which appears at about 31 °C, is assigned to the melting of the eutectic fraction, whereas the high temperature endotherm is attributed to the melting of either the H<sub>1</sub> or PEO solid solution. On the basis of thermal transitions of the H<sub>1</sub>/PEO system obtained from Figure 1, a typical eutectic phase diagram with a eutectic composition at 40/60 (H<sub>1</sub>/PEO) can be constructed as shown in Figure 4. The melting point of the eutectic mixture was about 31 °C. Since no eutectic melting was observed for samples with compositions of 95/5 and 90/10 (H<sub>1</sub>/PEO), a limited solid solution (designated as  $\beta$ ) is suggested in this region of the diagram. The tie line calculations based on the  $\Delta H$  at the eutectic melting of the blends show that the solid solution behavior may well extend to a composition close to 85/15 (H<sub>1</sub>/PEO). A small solid solution (H<sub>1</sub> in PEO) (assigned as  $\alpha$ ) is also suggested for samples of high PEO content. This was not observed experimentally, possibly because the H<sub>1</sub> content was too low to be detected. The liquidus line was determined by taking the minimum points of the melting endotherms plotted as shown in Figure 4. Above the liquidus line, PEO and  $H_1$  were in a well-mixed liquid state. The solidus line (dashed line) in the region rich in H<sub>1</sub> was qualitatively determined on the basis of the melting point onset. The eutectic isotherm on the solidus line was determined by the onset of the melting of the eutectic fraction. Below the eutectic isotherm, H1 and PEO should phase separate into two crystalline forms ( $\alpha$  and  $\beta$ ), though the segmental diffusion rate may be slow and the sample may slowly, if ever, reach an equilibrium state.

Figure 2 shows the thermograms of the H<sub>1</sub>/PTMO blends. The poly(tetramethylene oxide) macroglycol is different from poly(ethylene oxide) macroglycol in its lower content of ether groups, its lower melting point, and crystalline structure. As observed, pure PTMO displayed a melting point with an onset at 13 °C and a peak maximum at 23 °C. This was identified as the metastable melting point of PTMO (100 MW). The equilibrium melting point of high molecular weight PTMO was previously reported as having a peak maximum at 57 °C.17 Similar to the  $H_1/PEO$  system, the  $H_1/PTMO$  system possesses a eutectic phase diagram (Figure 5). The eutectic isotherm is at 10 °C, and the eutectic composition

Table I
Characterization of Polyether Macroglycols and Their Interaction Parameters with H,

sample	density	MW <sub>u</sub> <sup>a</sup>	$V_{iu}^{b}$	B, cal/cm³ c	$\chi_{12} d$	X 12 e	
 PEO	0.986	44.05	44.68	-4.63	-0.27	-0.26	
PTMO	0.976	72.11	73.88	-3.45	-0.33	-0.20	
PPO	1.004	53.08	52.87	-1.21	-0.08	-0.07	

<sup>a</sup> Molecular weight per polyether macroglycol repeat unit. <sup>b</sup> Molar volume per polyether macroglycol repeat unit. <sup>c</sup> Interaction density between  $H_1$  and polyether macroglycol per cm³ of polyether macroglycol. <sup>d</sup> Flory interaction parameter,  $BV_{1u}/RT$  at 120 °C. <sup>e</sup>  $\chi_{12}$  normalized by the molar volume of poly(ethylene oxide) macroglycol repeat unit at 120 °C.

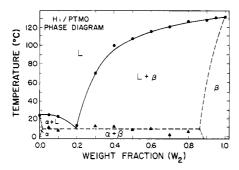


Figure 5. Phase diagram on the  $H_1/PTMO$  blend system. Liquidus points are shown by circles, and eutectic points by triangles. The solidus lines at both ends of the phase diagram are estimated.

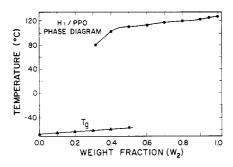


Figure 6. Phase diagram of  $\rm H_1/PPO$  blends. Melting points are shown by circles and glass transition points are shown by triangles.

is found to contain 20%  $H_1$ . This is less concentrated in  $H_1$  compared to the eutectic composition of the  $H_1/PEO$  system (40%  $H_1$ ). Compositions of  $H_1/PTMO$  at 95/5 and 90/10 showing no eutectic melting suggest that there is a solid solution in the region which is rich in  $H_1$ .

Figure 3 shows the thermograms of the  $H_1/PPO$  system. The PPO added was amorphous, having a  $T_g$  at -71 °C. It was noticed that as H<sub>1</sub> was gradually diluted with PPO, the melting point of H<sub>1</sub> decreased at a slower rate compared to the  $H_1/PEO$  and  $H_1/PTMO$  systems (Figure 6). As the amount of PPO was increased to a composition of 50/50 (H<sub>1</sub>/PPO), a distinct glass transition of PPO at -60 °C was observed in addition to the melting point of the hard segments. Further dilution with PPO caused the melting point of H<sub>1</sub> to disappear, the PPO glass transition temperature to appear at a lower temperature, and the  $\Delta C_{\rm p}$ in the transition zone to become larger. It was surprising that the presence of H<sub>1</sub> in PPO did not significantly affect the  $T_g$  of PPO, so that even with  $H_1/PPO$  in a ratio of 30/70 the  $T_g$  of PPO was only -64 °C ( $T_g$  of pure PPO = -71 °C). This suggests that the presence of  $H_1$  causes little hindrance of rotation in the PPO backbone in the amorphous mixture when the concentration of H<sub>1</sub> is less than about 50%. However at H<sub>1</sub> concentrations above 50%, the PPO may exist as a finely divided phase inclusion whose  $T_{\rm g}$  is not observable in the DSC experiment.

The melting point depression of H<sub>1</sub> caused by the addition of polyols in the mixture is similar to the melting

point depression observed in many other crystalline polymer-diluent systems. <sup>21,22</sup> The equilibrium mixing of  $H_1$  and polyols were analyzed by using the Scott equation. <sup>13</sup> The parameters used and results calculated are shown in Table I. For these systems the chemical potential,  $\mu'_{2u}$ , per mole of  $H_1$  unit in the mixture relative to its chemical potential  $\mu^{\circ}_{2u}$  in the pure liquid can be expressed as

$$\mu'_{2u} - \mu^{\circ}_{2u} = \frac{RTV_{2u}}{V_{1u}} \left[ \frac{\ln \phi_2}{M_2} + \left( \frac{1}{M_2} - \frac{1}{M_1} \right) \phi_1 + \frac{BV_{1u}}{RT} \phi_1^2 \right]$$
(5)

where the subscript 1 identifies the polyol and 2  $H_1$ ,  $\phi$  is a volume fraction,  $V_u$  is the molar volume of the repeating units, M is the degree of polymerization, and B is the interaction energy density of the  $H_1$ -polyol mixture. If the entropy of mixing can be neglected, the Flory-Huggins interaction parameter,  $\chi_{12}$ , is equivalent to  $BV_{1u}/RT$ .

The difference in the chemical potential between a crystalline  $H_1$  unit  $(\mu^c_{2u})$  and the same unit in the pure liquid state  $(\mu^o_{2u})$  can be written as

$$\mu^{c}_{2u} - \mu^{o}_{2u} = -(\Delta H_{2u} - T\Delta S_{2u})$$
 (6)

$$= -\Delta H_{2u} \left( 1 - \frac{T}{T_{m}^{\circ}} \right) \tag{7}$$

where  $\Delta H_{2\mathrm{u}}$  and  $\Delta S_{2\mathrm{u}}$  are the enthalpy and entropy of fusion per mole of  $H_1$  unit. The ratio  $\Delta H_{2\mathrm{u}}/\Delta S_{2\mathrm{u}}$  is assumed to be independent of temperature and equal to  $T^{\mathrm{o}}_{\mathrm{m}}$ , the equilibrium melting temperature. At the melting point of the mixture, the chemical potential of the  $H_1$  unit in the crystalline and liquid phases are identical so one obtains from eq 5 and 7

$$\frac{1}{T_{\rm m}} - \frac{1}{T_{\rm m}^{\circ}} = -\frac{RV_{2\rm u}}{\Delta H_{2\rm u}V_{1\rm u}} \left[ \frac{\ln \phi_2}{M_2} + \left( \frac{1}{M_2} - \frac{1}{M_1} \right) \phi_1 + \frac{BV_{1\rm u}}{RT} \phi_1^2 \right] (8)$$

To calculate B from eq 8, one must know the equilibrium melting point,  $T^{\rm o}_{\rm m}$ , the heat of fusion of  $\Delta H_{\rm 2u}$ , the density of  $\rm H_1$ , and the density of the polyols. To determine  $T^{\rm o}_{\rm m}$  of polymeric material experimentally, the Hoffman-Weeks method can be used. Unfortunately, since  $\rm H_1$  exists in a rather rigid phase, its diffusion rate may be too slow to maintain equilibrium during crystallization or ordering. This makes the Hoffman-Weeks method difficult to apply in order to obtain a vlaue of  $T^{\rm o}_{\rm m}$ . In this study, a  $T^{\rm o}_{\rm m}$  of  $\rm H_1$  (of 128.8 °C) was obtained by extrapolating the  $T_{\rm m}$  of the  $\rm H_1$ /polyol blends to zero polyol concentration. The  $\rm \Delta H^{\rm o}_{\rm 2u}$  of a hypothetically 100% crystalline sample of  $\rm H_1$  was determined to be 5.3 kcal/mol by applying Flory's equation (eq 9) to the melting temperatures of a series of monodisperse urethane oligomers<sup>22</sup>

$$\frac{1}{T_{\rm m}} = \frac{1}{T_{\rm m}^{\rm o}} + \frac{R}{\Delta H_{\rm 2u}} \frac{2}{M} \tag{9}$$

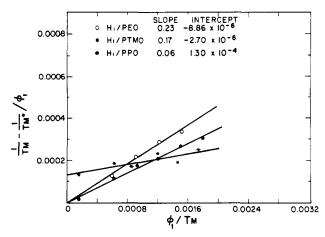


Figure 7. Plots of the quantity  $(1/T_{\rm m}-1/T_{\rm m}^{\rm o})/\phi_1$  against  $\phi_1/T_{\rm m}$  for  $\rm H_1/PEO,~H_1/PTMO,$  and  $\rm H_1/PPO$  systems.

where M is the degree of polymerization. The densities of  $H_1$ , PTMO, PPO, and PEO, measured at each samples melting point, were 1.298, 0.977, 0.986, and 1.004 g/cm<sup>3</sup>, respectively.

If the entropy terms can be neglected, eq 8 reduces to

$$\left(\frac{1}{T_{\rm m}} - \frac{1}{T_{\rm m}^{\rm o}}\right) / \phi_1 = -\frac{V_{\rm 2u}B\phi_1}{\Delta H_{\rm 2u}T} \tag{10}$$

In Figure 7, the data obtained in Figures 1–3 are plotted as  $(1/\phi)[1/T_{\rm m}-1/T^{\rm o}_{\rm m}]$  vs.  $\phi_1/T_{\rm m}$ . For the  ${\rm H_1/PEO}$  system, a least-squares fit of the data yields a straight line intersecting the vertical axis near zero. The slope of the straight line was 0.23 and the intercept was  $-8.8\times 10^{-6}~{\rm K}^{-1}$ . In view of the extremely small value of the ordinate intercept, the use of eq 10 appears justified. On the basis of values of  $V_{1u}$  of 44.68 cm<sup>3</sup>/mol,  $V_{2u}$  of 263.69 cm<sup>3</sup>/mol, and the slope, it was found that

$$B_{\rm H,/PEO} = -4.63 \text{ cal/cm}^3 \text{ (PEO)}$$

The Flory-Huggins interaction parameter,  $\chi_{12}$ , between H<sub>1</sub> and the repeating unit of PEO is -0.26 ( $\chi_{12} = BV_{1u}/RT$ ) at 120 °C.

In the system of  $\rm H_1/PTMO$ , the plot suggested by eq 10 yields a straight line with a slope of 0.17 and an ordinate intercept of  $-2.7 \times 10^{-6}$ . Again the small value of the ordinate intercept showed that the use of eq 10 was appropriate. The interaction density between  $\rm H_1$  and PTMO,  $B_{\rm H_1/PTMO}$ , was found to be -3.42 cal/cm³ (PTMO), and the  $\rm \chi_{12}$  between  $\rm H_1$  and the PTMO repeating unit,  $-(\rm CH_2)_4-O$ , ( $V_{1u}=73.88~\rm cm^3/mol$ ) was -0.32 at 120 °C. If the repeating unit of PTMO is chosen to have the same molar volume as the PEO repeating molar volume (44.68 cm³/mol),  $\rm \chi_{12}$  would be -0.20 at 120 °C.

In the system of  $H_1/PPO$ , the data which test eq 10 fall on a straight line intersecting the ordinate at  $1.29 \times 10^{-4}$  with a slope of  $6.08 \times 10^{-2}$ . The interaction density  $B_{H_1/PPO}$  was calculated to be -1.21. The  $\chi_{12}$  between  $H_1$  and the PPO repeating unit was -0.08 at 120 °C. If the repeating unit of PPO is normalized to have the same molar volume as the PEO repeating unit (44.68 cm³/mol), the value of  $\chi_{12}$  is -0.07 at 120 °C. Comparison of the data on all 3 systems reveals that the ordinate intercept in the  $H_1/PPO$  system was larger than that in the  $H_1/PTMO$  or  $H_1/PEO$  systems ( $\sim 10^{-4}$  vs.  $\sim 10^{-6}$ ). This may indicate that the entropy of mixing in the  $H_1/PPO$  system is more of a significant factor than in the other systems.

The negative value of  $\chi_{12}$  or B for all three systems indicated that the three polyols can form a thermodynamically compatible mixture above the melting point of

Table II Bragg Spacings for Crystalline H<sub>1</sub>, PEO, and PTMO As Calculated from the WAXD Patterns

material	$\begin{array}{c} \text{peak} \\ \text{position,} \\ 2\theta \end{array}$	Bragg spacing, Å	Bragg spacing a from ref 7, A					
H <sub>1</sub>	9.1 11.5 14.0 14.4 17.0 18.2 18.5 19.4 19.7 21.6 22.5 23.0 23.9 24.2 25.3	9.71 7.68 6.32 6.14 4.95 4.87 4.79 4.57 4.50 4.10 3.95 3.86 3.72 3.67 3.52	7.65 (004) 4.91 (102) 4.75 (101) 4.60 (014) 4.53 (106) 4.15 (107) 3.89 (102) 3.75 (018) 3.56 (103) 3.49 (119)					
PEO <sup>b</sup>	27.0 28.0 28.4 19.0	3.30 3.18 3.14 4.66	3.30 (104)					
PTMO <sup>b</sup>	23.3 $20.2$ $24.7$	3.82 4.40 3.60						

 $^a$  Calculated for given reflection plane assuming a triclinic unit cell with a=5.05 Å, b=4.67 Å, c=37.9 Å,  $\alpha=116^\circ,\,\beta=116^\circ,\,$  and  $\gamma=83.5^\circ$  as proposed for crystalline MDI/BD by Blackwell, Nagarajan and Hoitink (ref 7).  $^b$  Only the significant diffraction peaks of PEO and PTMO are reported.

 $H_1$ . The most negative value of B appeared in the  $H_1/PEO$  system, suggesting that there was a strong interaction between  $H_1$  and PEO. This could be due to PEO having a high concentration of ether oxygen which might interact with the urethane NH group in  $H_1$ . The PPO, which differs from PEO by having a methyl pendant group, showed the least interaction with  $H_1$ . This low interaction parameter could be due to a geometrical or conformational constraint caused by the methyl group on the PPO molecules which limits the intermolecular association.

Wide-Angle X-ray Diffraction. The interaction parameter densities in the blends were determined from the hard-segment melting point depressions by thermal analysis. This procedure is correct if the change in the free energy of the blend is solely due to mixing of the components and not to any crystalline transformation, change in the crystallite thickness, or a combination thereof. To confirm the validity of our analysis, the X-ray diffraction characteristics of the blends with respect to composition and temperature were studied.

The diffraction intensity was recorded from 3° to 40° (20). The locations of the diffraction maxima primarily serve to determine d spacings in the Bragg equation. The breadth of the diffraction peak is dependent on the size and perfection of the crystallites while the intensity is largely determined by the structure factors taking account of phase differences in the diffraction process. Figure 8 shows the wide-angle X-ray diffraction curves for pure H<sub>1</sub>, PEO, and PTMO. A list of the diffraction peaks is given in Table II. Many of the Bragg spacings H<sub>1</sub> possesses are very similar to those Blackwell observed for oriented MDI/BD hard segments. This match is expected, since H<sub>1</sub> is an analogue of the repeating unit of the MDI/BD segment. Blackwell reported the triclinic unit cell of

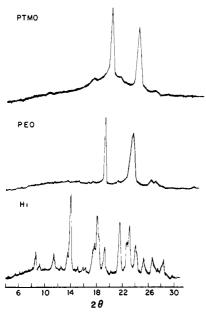


Figure 8. X-ray diffraction patterns of H<sub>1</sub>, PEO, and PTMO at 24 °C.

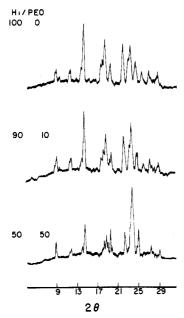


Figure 9. X-ray diffraction patterns of  $H_1/PEO$ : 100/0, 90/10, and 50/50.

MDI/BD to have the dimensions of a = 5.05 Å, b = 4.67 Å, c = 37.9 Å with  $\alpha = 116^{\circ}$ ,  $\beta = 116^{\circ}$ , and  $\gamma = 83.5^{\circ}$ . However, in the case of  $H_1$ , the unit cell may be altered due to the presence of numerous  $H_1$  chain ends. A higher degree of crystallinity is expected for  $H_1$  because its low molecular weight facilitates crystallization.

Figure 9 shows the wide angle X-ray diffraction curves for  $H_1/PEO$  samples at various compositions (100/0, 90/10, and 50/50). As suggested by the phase diagram, at ambient temperature  $H_1/PEO$  (90/10) is a solid solution ( $\beta$ ), while  $H_1/PEO$  (50/50) is a mixture of the two solid solutions,  $\alpha$  and  $\beta$ , in the ratio of 7 to 10. The X-ray diffraction patterns show both  $H_1$  and PEO diffraction peaks in the blend. It was also noticed that the addition of PEO caused no measurable change in the diffraction peak position or in the peak width of  $H_1$ . This provides a qualitative indication that the lamellar thickness of  $H_1$  crystallites is not reduced in the  $H_1/PEO$  blends, which supports the assumption upon which the calculation of the interaction parameter for  $H_1/PEO$  pairs is based. Figure

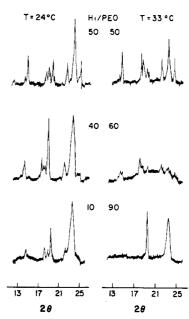


Figure 10. X-ray diffraction patterns of  $H_1/PEO$  samples at 24 and 33 °C.

10 shows the X-ray diffraction patterns of samples H<sub>1</sub>/ PEO (50/50, 40/60, and 10/90) at 24 and 33 °C which are below and above the eutectic point (31 °C). Each sample was conditioned at the desired temperature for 30 min before scanning. At 24 °C, both H<sub>1</sub> and PEO diffraction peaks were observed in all three compositions. This agrees with the phase diagram derived from thermal analysis, Figure 1, which suggests that these samples are a mixture of two crystalline phases,  $\alpha$  and  $\beta$ , in which  $\beta$  is mainly composed of  $H_1$  and  $\alpha$  primarily of PEO. As the temperature was increased from 24 to 33 °C, H<sub>1</sub>/PEO (50/50) exhibited only  $H_1$  diffraction peaks and  $H_1/PEO$  (10/90) only PEO diffraction peaks. This is because H<sub>1</sub>/PEO (50/50) and  $H_1/PEO$  (10/90) are on the opposite sides of the eutectic composition. At 33 °C, H<sub>1</sub>/PEO (50/50) transforms into a mixture of liquid and  $\beta$ , while  $H_1/PEO$ (10/90) changes into a mixture of liquid and  $\alpha$ . The X-ray diffraction is attributed to the solid solution ( $\alpha$  or  $\beta$ ) in both cases. It was also observed that  $H_1/PEO$  (40/60), which differs from the other blends by possessing only a single melting point at 31 °C, exhibits a largely suppressed H<sub>1</sub> diffraction pattern with no PEO diffraction characteristics at 33 °C. This indicates that  $H_1/PEO$  (40/60) is not the exact eutectic composition, although it is close to

Figure 11 shows the X-ray diffraction patterns of  $\rm H_1/\rm PEO$  (50/50) recorded at 24, 33, 43, 70, 90, and 100 °C. It can be observed that the PEO X-ray diffraction disappears at temperatures higher than 31 °C, while the  $\rm H_1$  X-ray diffraction slowly decreases with increasing temperature and finally vanishes at 100 °C. This is in agreement with thermal analysis. According to the phase diagram, the components of  $\rm H_1/\rm PEO$  (50/50) distribute between  $\beta$  and L phases in the ratio of 1/3, 1/4, 1/6, and 1/16 at temperatures of 33, 43, 70, and 90, respectively, and become all liquid at 100 °C, the liquidus point. It was also noticed that, among the diffraction peaks, those appearing at  $2\theta$  = 9, 14.4, 18.2, and 22.5° decreased at a slower rate with increasing temperature. This suggests that  $\rm H_1$  crystallites melt in a nonisotropic way.

Figure 12 shows the X-ray diffraction patterns of  $\rm H_1/PTMO~(50/50)$  and  $\rm H_1/PPO~(50/50)$ . At 24 °C  $\rm H_1/PTMO~(50/50)$  is a mixture of  $\beta$  and liquid in the ratio of 7/10. The X-ray diffraction peaks are solely attributed to the



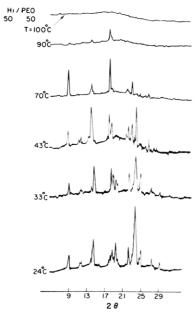


Figure 11. X-ray diffraction patterns of  $H_1/PEO$  (50/50) at 24, 33, 43, 70, 90, and 100 °C.

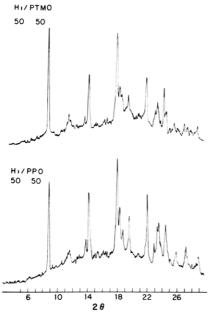


Figure 12. X-ray diffraction patterns of  $H_1/PPO$  (50/50) and  $H_1/PTMO$  (50/50) at 24 °C.

 $\beta$  solid solution, which is mainly composed of  $H_1$ .  $H_1/PPO$ (50/50) also has a two-phase morphology, consisting of  $H_1$ crystals and a PPO amorphous phase. In both cases, identical H<sub>1</sub> diffraction patterns were observed. This again shows that the presence of polyol leads to no unusual H<sub>1</sub> crystalline modification.

Optical Microscopy. An optical microscope was used to study the effect of composition on the crystalline texture and the size of spherulites found in crystalline blends. Samples were cast as thin layers on glass plates and dried at 24 °C in a vacuum oven for at least 1 day. Selected samples dried for periods from 1 to 7 days all showed similar morphology.

Figure 13 shows typical optical micrographs of H<sub>1</sub>/PEO polymer blends at the ambient temperature (24 °C). As can be observed in Figure 13a, the size of the H<sub>1</sub> spherulites varies from 10 to 100  $\mu$ m. In the blend where H<sub>1</sub> and PEO are in a ratio of 9/1 and form a solid solution (Figure 13b), the spherulites all have uniform texture and are observed

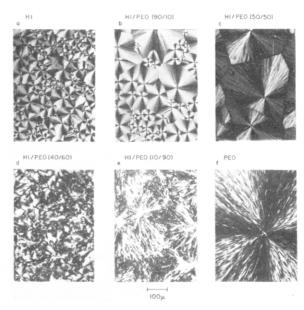


Figure 13. Optical micrographs of  $H_1/PEO$ : 100/0, 90/10, 50/50,40/60, 10/90, and 0/100 at 24 °C.

to range in size from 30 to 100  $\mu$ m, with the majority larger than 60  $\mu$ m. The spherulitic structure is also more welldefined and regular than the textures observed in samples of pure H<sub>1</sub>. Figure 13c shows a micrograph of the sample containing H<sub>1</sub>/PEO in a 50/50 ratio, in which the H<sub>1</sub> and PEO are distributed in two separated crystalline phases of  $\alpha$  and  $\beta$  in a ratio of 4/5. In this case an optical micrograph taken at 40 °C where the  $\alpha$  phase has melted showed that the sizes of the spherulites are the same as that in Figure 13c. Therefore it is believed that below the eutectic melting,  $\alpha$  and  $\beta$  crystal lamellae stack alternatingly in the form of radial fibrils growing from the spherulitic centers. It is important to note that there is only one spherulitic superstructure observable. Each spherulite is of the same texture and the spherulite size varies from 30 to 400  $\mu$ m. Most are above 200  $\mu$ m. The individual grains are in intimate contact with all adjacent grains so as to pack and fill space completely. Figure 13d is the micrograph of the sample of  $H_1/PEO$  (40/60), which contains  $\alpha$  and  $\beta$  in a ratio of 4.5/3.5 and is close to the eutectic composition as suggested by both WAXD studies and thermal analysis. This composition shows no welldefined spherulites. The birefringence observed is not distributed in any symmetric or regular pattern and is probably due to the fact that one is casting close to the eutectic composition where one would normally expect finely textured crystals.

Figure 13e shows the spherulitic structure of the  $H_1/$ PEO (10/90) blend, which is a mixture of  $\alpha$  and  $\beta$  phases, as suggested by X-ray diffraction. The spherulites have a different appearance than those described previously. Needle-type crystalline fibrils emanate radially from a nucleus. The bright fibrils are interspersed with dark regions, and no clearly defined grain boundaries can be observed. The spacing between two nuclei is about 200  $\mu$ m. Figure 13f shows the spherulites of pure PEO. The boundaries are sharp and all the spherulites are approximately 1600 µm in diameter.

The series of optical micrographs of the  $H_1/PEO$  blends showed that the size and texture of these mostly spherulitic samples change significantly with sample composition. The spherulite sizes were smallest in pure  $H_1$  and became larger and more well structured as the PEO was blended into  $H_1$ . The spherulite texture changed from  $H_1$ -like to PEO-like with an increasing amount of PEO, but there was

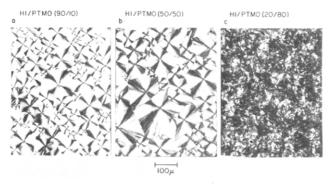


Figure 14. Optical micrographs of  $H_1/PTMO$ : (90/10), (50/50), and (20/80) at 10 °C.

basically only one type of spherulite observed at each blend composition. The increase in spherulite size indicates that the number of crystal nuclei decreases with the addition of PEO, suggesting that either nucleation is suppressed or that crystal growth is enhanced by the presence of PEO. Possibly, PEO enhances the diffusion of H<sub>1</sub> molecules, thereby increasing the rate of crystal growth. A comparison between pure H<sub>1</sub> and pure PEO shows that the spherulite size in PEO is at least 16 times larger than in H<sub>1</sub>. This could be attributed to the fact that crystallization at room temperature (24 °C) proceeded differently for each of the H<sub>1</sub> and PEO phases. At 24 °C, which is far below the  $T_{\rm m}$  of  $H_1$  (129 °C), nucleation of  $H_1$  is favored. The strong intermolecular forces such as hydrogen bonding in  $H_1$  allow the molecules to gather and align in small parallel arrays, which serve as crystal nuclei. Subsequently, the rigidity of the H<sub>1</sub> molecules may hinder its diffusion, resulting in slower growth. In the case of PEO, it may take longer to create a nucleus, because the crystallization temperature was closer to the  $T_{\rm m}$  of PEO (45 °C). However, in the case of PEO a higher segmental diffusion rate facilitates a higher crystal growth rate and thus larger spherulites.

Figure 14 shows the optical micrographs of three  $H_1/$ PTMO blends (90/10, 50/50, and 20/80). In order to be consistent with the microscopy carried out on the H<sub>1</sub>/PEO system, the optical micrographs were taken below the temperature of eutectic melting at  $\sim$ 6 °C ( $T_{\rm EU}$  =  $\sim$ 10 °C for  $H_1/PTMO$ ). At this temperature,  $H_1/PTMO$  (90/10) is a solid solution while both H<sub>1</sub>/PTMO (50/50) and (20/80) are a mixture of  $\alpha$  and  $\beta$  in the approximate ratio of 4/5 and 2/7, respectively. Similar to the H<sub>1</sub>/PEO system, the spherulites became larger and more regular as PTMO was blended with H<sub>1</sub>. As can be observed, the spherulite sizes of H<sub>1</sub>/PTMO (90/10) (Figure 14a) are mainly in the range between 50 and 130  $\mu$ m. Spherulite sizes of H<sub>1</sub>/PTMO (50/50) (Figure 14b) are between 100 and 200  $\mu m$ . It was also found that the fibers which radiate out from the spherulitic centers are in shorter segments and the appearance of birefringence is more diffuse in the  $H_1/PTMO$  (50/50) spherulites than in  $H_1/PTMO$  (90/10) spherulites. This is due to the difference in the distribution of  $\alpha$  vs.  $\beta$  phase between H<sub>1</sub>/PTMO (50/50) and  $H_1/PTMO$  (90/10). Figure 14c shows the micrograph of  $H_1/PTMO$  (20/80), which is close to the eutectic composition. Similar to H<sub>1</sub>/PEO (40/60), the birefringence exhibits an irregular pattern, and no spherulites are observed.

Figure 15 shows the optical micrographs of  $H_1/PPO$  (10/90) and  $H_1/PPO$  (50/50) at 24 °C. At this temperature, both  $H_1/PPO$  blends possess crystalline and amorphous phases in contrast to  $H_1/PEO$  or  $H_1/PTMO$  systems which are composed of two crystalline phases. The same features found in the blend systems of  $H_1/PEO$  and

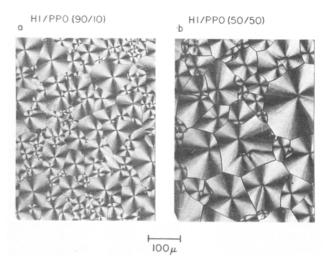


Figure 15. Optical micrographs of H<sub>1</sub>/PPO: (90/10) and (50/50) at 24 °C.

 $H_1/PTMO$  were observed. The spherulites became larger and more well developed as the poly(propylene oxide) was blended with  $H_1$ .

It is understood that the larger the grain size of the spherulites the smaller the amount of grain boundary and the lower the grain boundary energy. Thus, the stability of the crystal is increased as polyol is blended into  $H_1$ . However, the miscibility of  $H_1$  and the polyol also affect the melting point by lowering the blend's enthalpy in the liquid state. A careful comparison reveals that the increase in the size of spherulites by the addition of PTMO or PPO is not as substantial as the addition of PEO to  $H_1$ . This suggests that the spherulite radial growth rates are more rapid when  $H_1$  is blended with PEO than with PTMO or PPO. In general, the spherulitic growth rate can be qualitatively described by the Lauritzen and Hoffman equation (eq 11), which originated from the modified Turnbull–Fisher equation<sup>23,24</sup>

$$G = G_0 \exp[-U^*/R(T - T_{\infty})] \exp(-\Delta \phi^*/RT)$$
 (11)

where G is the radial growth rate, and  $U^*$  is the activation energy for transport of crystallizable segments through the liquid to the site of the crystal.  $T_{\infty}$  is a hypothetical temperature where all molecular motion associated with viscous flow ceases and is related to  $T_g$  by  $T_{\infty} = T_g - C$ , where C is a constant.  $\Delta \phi^*$  is the free energy required to form a critical size nucleus from the liquid and  $G_0$  is a constant related to the initial composition. For the blends which are richer in H<sub>1</sub> than the eutectic composition, the presence of polyol has two significant effects on the process of crystallization. First, it lowers the activation energy,  $U^*$ , for transport of crystallizing units H<sub>1</sub> across the liquidcrystal interface. Second, the polyol dilutes the H<sub>1</sub> and weakens the interaction between H<sub>1</sub> molecules, causing the need for an extra amount of energy in order to gather enough H<sub>1</sub> molecules to form a nucleus of critical size. This explains why the size of the spherulites increases as polyols are mixed into H<sub>1</sub>.

#### Conclusions

The urethane hard-segment model compound  $H_1$ , diethyl 4,4'-methylenebis(N-phenylcarbamate), can serve as an analogue of the repeating unit of MDI/BD hard segments in conventional polyurethane block copolymers. DSC studies reveal that blends of  $H_1$  and PEO give rise to a eutectic composition at a weight ratio of  $\sim 40/60$  ( $H_1/PEO$ ) with  $T_{\rm ME}=31$  °C.  $H_1$  and PTMO also form a eutectic at about 20/80 ( $H_1/PTMO$ ) with  $T_{\rm ME}=10$  °C.

According to the Flory-Huggins theory, the higher the degree of polymerization of the polyol and the lower the value of the  $\rm H_1$ -polyol interaction parameter, the higher the polyol concentration as well as  $T_{\rm ME}$  of the eutectic composition. In contrast to the PEO and PTMO systems, poly(propylene oxide) (PPO) is intrinsically an amorphous compound and forms a crystalline-amorphous phase diagram with  $\rm H_1$ .

Wide angle X-ray diffraction revealed that the presence of the polyol, as well as variations in temperature up to the liquidus point, did not alter the crystal form of  $H_1$ . This suggests that the melting point depression observed is a result of the excess free energy released during mixing, which allows determination of the  $H_1$ /polyol interaction parameter using Scott's equation. The interaction parameter densities of  $H_1$ /polyol pairs at their melting points were found to be  $B_{H_1/\text{PEO}} = -4.63 \, \text{cal/cm}^3$ ,  $B_{H_1/\text{PTMO}} = -3.41 \, \text{cal/cm}^3$ , and  $B_{H_1/\text{PPO}} = -1.21 \, \text{cal/cm}^3$ . The negative values of B indicate  $H_1$  and the polyols (PEO, PTMO, and PPO) form compatible liquids.

The morphology of  $H_1$ /polyol blends was studied with a polarizing microscope. Distinct spherulites were observed for pure  $H_1$  and  $H_1$ /polyol blends. With the addition of polyols, the spherulite radii increase and the texture of the spherulites change from maltese cross patterns to radiating fibrous morphologies, especially for those blends that are of high PEO or PTMO content. The spherulites of  $H_1$ /PEO systems are larger in size than those of  $H_1$ /PTMO or  $H_1$ /PPO. This may be due to the fact that  $H_1$  and PEO possess a strong interaction (suggested by the low value of  $B_{H_1/PEO}$ ) which makes PEO a more effective diluent for hindering nucleation in  $H_1$ . In addition, the presence of PEO may also ease the transport of the crystallizing  $H_1$  units across the liquid–crystal interface, resulting in larger spherulites.

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**Registry No.** H<sub>1</sub>, 10097-16-2; PEO, 25322-68-3; PPO, 25322-69-4; PTMO, 25190-06-1.

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Miscibility of Ethylene-Vinyl Acetate Copolymers with Chlorinated Polyethylenes. 3. Simulation of the Spinodal Using the Equation of State Theory

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ABSTRACT: Chlorinated polyethylene and ethylene-vinyl acetate copolymers have previously been shown to be miscible and to phase separate on heating. In this paper a spinodal equation based on Flory's equation of state theory was derived and applied to the phase diagrams of these mixtures. Using values of the interactional parameter,  $X_{12}$ , derived from heats of mixing measurements, it was found that the predicted spinodal curves could not match the cloud point curves unless the entropy correction term containing  $Q_{12}$  was used. Also the predicted curves were flatter than the cloud points, suggesting an overestimation of  $X_{12}$ . The excess volume change on mixing was also calculated and was found to be larger than the measured value. This can also be improved by introducing  $Q_{12}$  and by using a lower value of  $X_{12}$ .

#### Introduction

In previous papers we have described the miscibility of various ethylene-vinyl acetate copolymers (EVA) with chlorinated polyethylenes (CPE).<sup>1,2</sup> This was demonstrated by the presence of single glass transition temper-

atures intermediate between those of the pure polymers. We also have measured the cloud point curves of the mixtures.<sup>1</sup> They phase separate on heating, showing a lower critical solution temperature (LCST). The LCST was higher for polymers with a higher content of vinyl